To: P. Lin, P. Broberg and Mr. Joe Fortney

From: Gary Atchison

Date: 2/22/10

Re: Forming Die Test Press Design Project Report

<u>Report Outline</u>

- Report Summary
- Problems and Corrections
- Status of the Machine
- Timeline for Completion
- Supporting Information
 - System Block Diagram
 - Project Gantt Chart
 - Hydraulic Power Unit Calculations
 - Motion Controller Information Calculations

Report Summary

Gentlemen, what you will find in the following report are updated screen shots of my project Gantt chart, the system calculations for the hydraulic power unit required for the machine and the MMC Standalone control setup file calculations. Also is a brief description of any issues that have come up along the way and their corrections, what is the status of the machine and what is left to be done. I would like to note that this machine has had an Ethernet module installed on the MMC Standalone control that will allow us to connect remotely from Marion with the machine in Germany. This will allow us to be able to modify and download control programs if needed without making a trip to Germany.

Problems and Corrections

The original electrical design of the machine was done a year ago before the hydraulic system was designed so the intention was to use the hydraulic system design of the first test press machine. It did not have a cooling fan motor on the hydraulic unit. Instead it used 2 electrical enclosure cooling fans mounted around the hydraulic unit to help cool it. Because we wanted to improve the design of the hydraulic power unit a cooling fan was included so we had to update the electrical design to include the hydraulic power unit cooling fan.

Another problem that has arose because of the changing the hydraulic power unit design from that of the original test press design is with the new design we changed from a hydraulic servo valve which uses a current input to a proportional valve which uses a voltage input. Because of this, the electrical system has been updated which requires another 24V power supply for the proportional valve and the removal of the VC2124 which was going to be used to convert the analog +/- 10V signal to a current which the servo valve used. We are currently awaiting the

arrival of the power supply so it can be installed. At that time we will remove the VC2124 converter and complete the wiring as necessary.

There was some confusion when parts were ordered for the hydraulic system and the wrong length cylinder and linear transducer were ordered. Parts were ordered for a 10 inch cylinder instead of a 15 inch cylinder. A 15 inch cylinder and a 15 inch MTS linear transducer have been ordered and are expected to arrive any time.

Status of the Machine

Presently the machine has been built allowing the installation of the hydraulic power unit and the electrical enclosure. Hoses are being routed to length so that they can be crimped. The safety pin cylinder has been installed and guards are in the process of being installed. Most of the electrical installation has been done but does not include the installation of the outputs solenoids for air control. The MS Project Gantt chart has been updated to reflect the recent progress on the machine and a document containing the calculations for the hydraulic power unit and the motion control system has been created.

What is left to be done is to complete the hydraulic hose installation and the machine wiring at which time we can begin installing the programs for the operation of the machine. Once these are complete we can begin testing and debug of the various systems. Once testing and debug are complete we can fully run the machine to make sure that all requirements have been met.

<u>Time Line for Completion</u>

Present: 2/19/10 Finish electrical and hydraulic installation: 3/1/10 Finish the installation of interlocks and guards: 3/1/10 Testing and Debug complete by: 3/15/10 Ship the Machine: 3/15/10 to 4/15/10 depending on machine schedule

Supporting Information

What you will find in the following information is the information for the system design, including hydraulic and motion control calculations. These will be included in the final report at the end of the semester. You will also find a block diagram that shows the basic system components and how they are connected to create a complete system. The only updated Gantt chart that will be shown are those with recent activity and those to yet be completed. I will begin on the next page with the System Block Diagram and I will provide subheadings for clarity.

System Block Diagram:



Figure 1 System Block Diagram showing interconnectivity of all components

Gantt Charts:

	0	Task Name	Duration	Start	Finish	Resource Names
1	1	Analysis	30 days	Mon 2/9/09	Thu 3/19/09	
2	1	Analyze Existing Program	1 day	Mon 2/9/09	Mon 2/9/09	Gary Atchison,Roger Beck
3	1	Review Controls and VO Opertion in Existing Sequential Code	1 day	Mon 2/9/09	Mon 2/9/09	Gary Atchison
4	1	Analyze Existing Controls	1 day	Mon 2/9/09	Mon 2/9/09	Gary Atchison[18%].Roger Beck
5	1	Review Existing Controls Usage and Wiring Schematics to determine what is needed	1 day	Mon 2/9/09	Mon 2/9/09	Roger Beck.Gary Atchison
6	1	Compare Detta Computer System with G&L Controls MMC to determine brand of Controls	1 day	Mon 2/9/09	Mon 2/9/09	Roger Beck.Gary Atchison
7	1	Order New Control System	30 days	Mon 2/9/09	Thu 3/19/09	Gary Atchison[17%].Roger Beck
8	10	Place order for control system components and electrical parts	30 days	Mon 2/9/09	Thu 3/19/09	Gary Atchison Roper Beck
9	× ~	Developing the New Control System	38 days	Wed 2/11/09	Wed 4/1/09	Roger Beck Gary Atchison
10	1	Create New Electrical Drawings	5 days	Tue 2/24/09	Mon 3/2/09	Roger Beck
11	×	Create New Ladder Program	21 days	Wed 2/11/09	Tue 3/10/09	Gary Atchison
12	×	Mock Up Control System to test Communication	1 day	Wed 4/1/09	Wed 4/1/09	Gary Atchison
13	*	Progress Report 1	1 day	Thu 9/10/09	Thu 9/10/09	Gary Atchison
14	1	Progress Report 2	1 day	Thu 10/1/09	Thu 10/1/09	Gary Atchison
15	1	Progress Report 3	1 day	Thu 10/22/09	Thu 10/22/09	Gary Atchison
16	×.	Progress Report 4 Initial Proposal and 10 minute presentation	1 day	Thu 11/19/09	Thu 11/19/09	Gary Atchison
17	×.	Final FCFT 490 Report and Presentation	1 day	Thu 12/10/09	Thu 12/10/09	Gary Atchison
18	×.	Develop and Order Hydraulic System	62 days	Thu 10/22/09	Tue 1/12/10	loe Fortney & LL indvall
19	×	Create New Hyd Sytem Design	18 days	Thu 10/22/09	Fri 11/13/09	All indvall loe Fortney
20	*	Order Hyd System	45 days	Fri 11/13/09	Tue 1/12/10	
21	Y	Building the Press and Installing Components	25.38 dave	Mon 1/11/10	Thu 2/11/10	Assembly Department Electrical Department
22	./	Paint the machine structure	1 day	Mon 1/25/10	Mon 1/25/10	Assembly Department
23	*	- Build the Press	14 75 dave	Mon 1/25/10	Thu 2/11/10	Assembly Department
24	1	Assemble the Forming Head	1 day	Mon 1/25/10	Man 1/25/10	Assembly Department
25	*	Install Brase Forming Head to Quide Din Bushings	1 day	Eri 2/5/10	Eri 2/5/10	Assembly Department
20	✓	Install Guarda and Interlacking Machanisma	2 days	Mon 2/9/10	Tue 2/0/10	Assembly Department
20		install Guards and Interlocking Mechanisms	2 days	Tuo 2/0/10	Wed 2/10/10	Assembly Department
21		Install Budraulia Cylinder and Linear Transducer	2 udys	Tue 2/9/10	Tuo 2/0/10	Assembly Department
20		Install Hydraulic Cylinder and Einear Transducer	2 days	Wed 2/10/10	Thu 2/11/10	Assembly Department
20		Install Hydraulic Hoses, check valves any remaining components	2 uays	Web 2/10/10	Fri 4/22/40	Electrical Department
31	1	Install Electrical Components	10.50 days	Mon 1/11/10	Tuo 1/12/10	Electrical Department
51	à	Task Name	Duration	Start	Finish	Resource Names
22	-			5-14/00/44	5-14/00/40	Orea Mathian Barra Barla
32	¥	Added Cooling Fan Output to Ladder code and Drawings	1 day	Fri 1/22/10	FR 1/22/10	Gary Atchison, Roger Beck
33	 ✓ 	Install Controls Components such as MMC, Ethernet Module, SAB, VO Blocks	1 day	Wed 1/13/10	wed 1/13/10	Electrical Department
34	×	Install Heat Controls	1 day	Thu 1/14/10	Thu 1/14/10	Electrical Department
35	×	Install Operator Interface	1 day	Thu 1/14/10	Thu 1/14/10	Electrical Department
30		Run and attach all wiring	3 days	Thu 1/14/10	Mon 1/16/10	Compartment
20	*	Progress Report Due January 25, 2010	1 day	Mon 1/25/10	Mon 1/25/10	Gary Atchison
20	¥	Updated Progress Report Due by 5:00pm 1-25-10	1 day	Mon 1/25/10	Mon 1/25/10	Gary Atchison
39	×	updated Flow Diagrams for clarity, created paint documents and inserted into the proposal	1 day	Mon 1/25/10	Mon 1/25/10	Gary Atchison
40	¥	Added summary, updated Table of Contents, added departments to Resources	1 day	Mon 1/25/10	Mon 1/25/10	Gary Atchison
41	¥	Einsteinen Benert Due Erstemmen 4. 2040	1 day	Mon 1/25/10	Mon 1/25/10	Gary Atchison
42	*	Dreaman Depart #1 Diage II Due by 5:00em 2 1 10	1 day	Mon 2/1/10	Mon 2/1/10	Gany Atchings
43	*	Progress Report #1 Phase II Due by 5:00pm 2-1-10	1 day	Mon 2/1/10	Mon 2/1/10	Gary Atchison
44	*	Add summary for any new changes and ar medifications, review requirements	i uay	Mon 2/1/10	Mon 2/1/10	Cary Atchison
45	*	Design Depart (2nd Depart) Due by 5:00nm 2 22 10	1 day	Mon 2/0/00	Mon 2/0/00	Gany Atchison
47	~	Installing Hydrauliae and Starting Up the Machine	202 06 days	Mon 2/9/09	Fri 2/40/40	Assembly Department
48	1	Installitydraulic System to the Machine	3 dave	Mon 2/15/10	Wed 2/17/10	Assembly Department
40	*	Statun New Control System	209 06 dave	Mon 2/9/09	Fri 2/40/40	Capy Atobiaon
50	1772	Dowolaad Operator Interface Program	1 day	Mon 2/1/10	Mon 2/1/10	Cary Atchison
51	100	Download the machine program (Ladder)	1 day	Mon 3/1/10	Mon 2/1/10	Capy Atchison
52	100	Establish Communication with MMC remotely using DicPro for Internet Downloading	1 day	Mon 3/1/10	Mon 3/1/10	Gany Atchison
53	10	Eatablish Communication with mill Control (Accel Decel Velocity and Head Onen Decitions)	3 dave	Mon 3/8/10	Wed 3/10/10	Consultant Cany Atchison
54		Test Operator Interface Communication (k it communication with the ladder)	J days	Tue 3/2/10	Tue 2/2/40	Gany Atchison
55	100	Test heat Control and estim nargenters for the heat	1 dest	Wed 3/2/10	Wed 3/2/10	Gary Atchison
56	Let .	Test I/O Operation	1 day	Mon 2/9/09	Mon 2/0/00	
57		Solenoid Operation /Top Dis Air, Bottom Dis Air)	1 day	Mon 2/9/09	Mon 2/0/00	
58		Diat Light Operation (Top Die All, Dollon Die All)	1 day	Mon 2/9/09	Mon 2/0/09	
50	-	- mor Light Operation (Fower on, Run mode, Manual Mode, Lock Mills Retracted, Lock Pins Extended)	2 06 days	Thu 3/44/40	Fri 2/43/09	Cany Atchieon
60	1772	Teet Quard Oneration	2.00 days	Thu 3/11/10	Thu 3/11/10	Gany Atchison
61		resi ouaro operation Taet Palm Button Operation	1 day	Thu 3/11/10	Thu 3/11/10	Gary Atchison
62		Test Operation of the AutoManual Mode Switch	1 day	Thu 3/11/10	Thu 3/11/10	Gary Atchison
52	1000	rest operation of the Automatival mode SWICH	ruay	110 3/11/10	1110 3/11/10	

	0	Task Name	Duration	Start	Finish	Resource Names
63		Can we only start the hydraulics in Manual Mode using the Simultaneous Press of the Palm Buttons?	1 day	Thu 3/11/10	Thu 3/11/10	Gary Atchison
64		Can the accumulator only be charged when the guards are closed?	1 day	Fri 3/12/10	Fri 3/12/10	Gary Atchison
65		Does the accumulator only charge in Auto Mode?	1 day	Fri 3/12/10	Fri 3/12/10	Gary Atchison
66	111	Do the safety Pins engage when the sliding guard door is opened?	1 day	Fri 3/12/10	Fri 3/12/10	Gary Atchison
67		Test the 8 Operations of the machine as described in the flow diagrams	3.13 days	Mon 3/15/10	Wed 3/17/10	Gary Atchison
68	111	Locking Pins Operation	1 day	Mon 3/15/10	Mon 3/15/10	Gary Atchison
69	11	Going to Start Position	1 day	Mon 3/15/10	Mon 3/15/10	Gary Atchison
70		Hydraulic Startup	1 day	Mon 3/15/10	Mon 3/15/10	Gary Atchison Gantt Chart Sheet 2 1-22-
71	111	Homing the Machine	1 day	Tue 3/16/10	Tue 3/16/10	Gary Atchison
72	11	Going to Start Position based on the Program Selected (1-4) from the HMI	1 day	Tue 3/16/10	Tue 3/16/10	Gary Atchison
73		Cycle Start (Machine Start)	1 day	Tue 3/16/10	Tue 3/16/10	Gary Atchison
74	111	Manual movement of the head (Jogging)	1 day	Wed 3/17/10	Wed 3/17/10	Gary Atchison
75		Heat Control	1 day	Wed 3/17/10	Wed 3/17/10	Gary Atchison
76		Test Motion Control and perform debug of motion control until proper control is established	2 days	Thu 3/18/10	Fri 3/19/10	Gary Atchison
77	111	Test functionality of the overall systems for proper operation (All systems working together)	1 day	Fri 3/19/10	Fri 3/19/10	Gary Atchison
78	111	Do we meet the requirements for Safety, EC, Electrical and System	1 day	Fri 3/19/10	Fri 3/19/10	Gary Atchison
79		System Construction and Unit Testing Report (3rd Report)	1 day	Mon 3/22/10	Mon 3/22/10	Gary Atchison
80		First Testing Report Due 5:00pm 4-5-10 (4th Report)	1 day	Mon 4/5/10	Mon 4/5/10	Gary Atchison
81		Second Testing Report Due 5:00pm 4-12-10 (5th Report)	1 day	Mon 4/12/10	Mon 4/12/10	Gary Atchison
82		E Progress Report and Design Review	14.63 days	Tue 4/13/10	Fri 4/30/10	
83		Final Report Writing	4 days	Tue 4/13/10	Fri 4/16/10	Gary Atchison
84	-	Final Project and Presentation	5 days	Mon 4/26/10	Fri 4/30/10	Gary Atchison

Figure 2 Gantt Chart updated to show recent and future activity

Hydraulic Power Unit Calculations:

The following given parameters will be used to make hydraulic calculations to simulate a production speed of 40 SPM:

Time to Retract = 350ms Time to Extend = 350ms Closed Dwell = 500ms

Note:

Because this machine does not run in a continuous mode, open dwell is not considered in the calculation for head speed. Time to retract plus time to extend plus closed dwell as noted yield a 50 SPM machine rate. If we added an open dwell of 300ms then it would be equal to a 40SPM machine.

Head Open Position 11.375 inches – Die Shut Height 7.25 inches = 4.125 inch head stroke

Forming Pressure required = 20,000 pounds forming force

Head weight with components (HW) = 1250 pounds head + 110 pounds components = 1360 pounds

Friction Force (FF) = $.24*HW*cos(0^{\circ}) = .24*1360*1 = 326.4$ pounds

The pages following are the calculations to be used in the development of the Forming Die Test Press based on the above given conditions:

AverageVelocity(Va) = 4.125 inches / .350 ms = 11.78 inches / sec ondFinalVelocity(Vf) = 2 * S ÷ t = (2 * 2.0625 inches) ÷ .175 sec = 23.6 inches / sec ond Using the distance and time under acceleration

Where S = Distance moved in inches = 2.0625 inches

t = Time of acceleration = .175 seconds



Maximum Oil Flows:

Cylinder Bore = 3.25 inches Cylinder Rod = 2 inch diameter $CRA = CylinderRodArea = \pi * r^2 = 3.14 * 1.0^2 = 3.14 inches^2$ $CPAE = CylinderPistonAreaExtending = \pi * r^2 = 3.14 * 1.625 inches^2 = 8.3 inches^2$ $CPAR = CylinderPistonArea Re tracting = CPAE - CRA = 8.3 inches^2 - 3.14 inches^2 = 5.16 inches^2$

Oil Flow to Extend (OFE):

 $OFE = CPAE * Vf = (8.3in^2 * 23.6in / sec) = (195.9in^3 / sec) * (60 sec/min) = (11754in^3 / min) / (231in^3 / gal) = 50.9gal / min$

Oil Flow to Retract (OFR):

 $OFR = CPAR * Vf = (5.16inches^2 * 23.6in / sec) = (121.8inches^3 / sec) * (60 sec/min) = (7308inches^3 / min) / (231inches^3 / gal) = 31.6gal / min$

Hydraulic Oil Pressure Required to generate 20,000 pounds of forming force (HOPR):

 $HOPR = For \min gForce \operatorname{Re} quired / CPAE = 20000 / 8.3 inches^2 = 2410 pounds / inches^2$

Weight of the Head and Components (HW) + Friction Force (FF)

HW + FF = 1360 pounds + 326.4 pounds = 1686.4 pounds

Find the amount of hydraulic pressure required to accelerate the head upward (PAHU):

To accelerate the 1686.4 pounds of the head at a production speed: "Use the formula"

a = acceleration rate S = distance moved in inches t = time of acceleration in seconds $a = (2*S)/t^2$ $a = (2*2.0625 inches)/.175 \sec^2 = 134.7 inches/\sec^2$

Convert acceleration to feet/sec:

 $a/12inches = (134.7inches/sec^{2})/12 = 11.23 feet/sec^{2}$

As well as knowing acceleration we also need to know (**R**) which is the Resultant Force On the Body. To find (**R**) use the following formula:

 $\begin{array}{l} R = Resultant \ Force \ on \ the \ Body \\ w = HW + FF \\ g = Gravitational \ Force \ (32.16 \ feet/sec^2) \ or \ (9.81 meters/sec^2) \\ a = acceleration \ rate \ in \ feet/sec^2 \end{array}$

R = (w/g) * a = 1686.4 pounds / (32.16 ft / sec²) = 52.4 footpound / sec²(52.4 footpound / sec²) * (11.23 ft / sec²) = 587.9 pounds W = R + w = 587.9 pounds + w = 587.9 + 1686.4 pounds = 2274.3 pounds

To finish finding hydraulic pressure need to accelerate the head upward: Use the flowing formula for Pressure to Accelerate Head Upward (PAHU): $PAHU = W / CPAR = (2274.3 \, pounds) / (5.16 \, inches^2) = 441 \, pounds / in^2$

Note:

Accumulator Pressure must be greater than or equal to the Forming Pressure (HOPR), which is 2410 pounds/inch² because pressure is required from the accumulator for movement of the forming head.

To find the amount of pressure required for the accumulator pre-charge we must know and do the following:

1) The largest volume of oil taken from the accumulator will be at the maximum amount of head stroke (HS) which is:

Four head open positions will be needed: 20.375 inches 17.375 inches 14.375 inches 11.375 inches

Two different shut heights (closed die height) will be used for the dies: *12 inch 7.25 inch*

12 inch shut height will be used with the 20.375 inch and 17.375 inch Machine Head Open Position

7.25 inch shut height will be used with the 14.375 inch and 11.375 inch Machine Head Open Position

The greatest head travel is realized when using the 20.375 inch Head Open Position with the 12 inch shut height die, so;

HS(HeadStroke) = 20.375inch - 12inch = 8.375inches

2) The oil volume required from the accumulator to move the head 8.375 inches is found by the following:

Extending:

 $HS * CPAE = 8.375 inch * 8.3 in^2 = 69.5 in^3$

This 69.5 inches³ is compressed to 2410 pounds/inch² We need to know that .5% oil volume compression/1000 psi is: 2410 psi/1000 psi/.005 = 2.41*.005 = 1.205% or .01205

Now we can finish finding oil volume from the accumulator (OFA) to move the head 8.375 inches

 $OFA = (HS * CPAE) * .01205 = .84in^{3} + (HS * CPAE) = 70.34in^{3}$ $OFA = 69.5 * .0125 = .84 + 69.5 = 70.34in^{3}$ *Now we can find the amount of pressure required for the accumulator pre-charge* Use the equation: $P_1 * V_1 = P_2 * V_2$

Where:

$$\begin{split} P_1 &= HOPR = 2410 \, pounds \, / \, inches^2 \\ P_2 &= Accumulator \, Pre\text{-}charge \, Pressure \\ V_1 &= Rated \, Gas \, Volume = 1124 in^3 \\ V_2 &= V_1 - OFA = 1124 in^3 - 70.34 in^3 = 1053.7 in^3 \end{split}$$

 $P_2 = (P_1 * V_1) / V_2 = (2410 * 1124) / 1053.7 = 2708840 / 1053.7 = 2570.8 \, psi$ Accumulator Pressure

PVR = Pump Volume Required at a 4.125" stroke P = Pump = 4gallons/minute Stroke = 4.125 inches

A = Cylinder Volume Extending B = Cylinder Volume Retracting

 $A = CPAE * Stroke = 8.3 inches^{2} * 4.125 inches = 34.24 inches^{3}$ $B = CPAR * Stroke = 5.16 inches^{2} * 4.125 inches = 21.29 inches^{3}$ $PVR = A + B = 34.24 + 21.29 = 55.53 inches^{3}$ PVR Converted to gallons = .24 gallons

TTR = Time Required to Refill the Accumulator at a 4.125" stroke

TTR = .24 gallons required at .066 gallons/second (4gallonsl/minute) = 3.64 sec

M = *Motor* Size Required

$$\begin{split} P &= Pump = 4 gallons/minute \\ P_2 &= 2571 pounds/inches^2 \\ K_1 &= 1714 \\ K_2 &= .85 \end{split}$$

$$\mathbf{M} = \frac{P_2 * P}{K_1 * K_2} = \frac{2571 * 4}{1714 * .85} = 7.06 HorsePower$$

We will use the common size 10HorsePower motor

The volume of oil required to manually move the forming head at 1 inch/sec is as follows:

To manually extend the head: $1gallon = 231inches^{3}$ $CPAE * 1inch = 8.3inches^{3}$ $8.3inches^{3} / 231inches^{3} = .036gallons / sec ond$ (.036gallons / sec ond) * (60 sec onds / 1) = 2.16gallons / min ute

Using a 4-gallons/minute pump, the velocity that can be achieved manually extending the head 1inch/second:

 $4 gallons / \min ute / 2.16 gallons / \min ute = 1.85 inches / \sec ond$

To manually retract the head: $1gallon = 231inches^{3}$ $CPAR * 1inch = 5.16inches^{3}$ $5.16inches^{3} / 231inches^{3} = .023gallons / sec ond$ (.023gallons / sec ond) * (60 sec onds / 1) = 1.34gallons / min ute

Using a 4 gallons/minute pump, the velocity that can be achieved manually retracting the head 1inch/second:

4gpm/1.34gpm = 2.98inches/second

Motion Controller Information Calculations:

The setup information for the motion controller to make its calculations requires the following input data.

Resolution to be used for calculations = .00025 inch

Axis Data:

Output Type = D/A Input Type = Encoder Output Slot Channel = 1.1 Input Slot Channel = 1.1 Encoder Driver = Differential Encoder Type = Quadrature

Scaling Data Requires:

Input Scaling:

Feedback Units = 4 (4*resolution to = .001" of an inch = 4*.00025 = .001 inch) Ladder Units = 1 (1LU = .001 inch so values in the ladder to = 1 inch are * 1000) So 4 inches in the ladder = 4000 Ladder Units/Axis Units = 1 (These are the units of measurement for the system and must be integers, at 1 no further scaling is needed)

Output Scaling:

Commanded Voltage = 10000 mv (This is equal to 10V which is the analog signal the Controller outputs) Motor RPM at Voltage = 23.6 inches/second or 1416 inches/minute (This is our calculated *Vf*) Counts/Motor Rev = 4000 pulses/inch (Based on the resolution, 4000*.00025 = 1 inch)

Iterator Data:

Velocity Limit = $\frac{Vf * (Counts / Mtr \text{Re }v) * (AU / LU) * (LU / FU)}{1416 * 4000 * 1 * (1/4) = 1,416,000 AU / \min ute}$

Acceleration Ramp = $\frac{VelocityLimit / t =}{1416000 / .175 = 8,091,428AU / \min ute / \sec ond}$

Deceleration Ramp = $\frac{VelocityLimit / t =}{1416000 / .175 = 8,091,428AU / \min ute / \sec ond}$

Controlled Stop Ramp = $\frac{VelocityLimit / t * 10^{1} =}{1416000 / .175 = 80,914,280 AU / \min ute / \sec ond}$

Move Accel/Decel Max Accel = $\frac{(3/2) * VelocityLimit / 3 \sec onds}{(3/2) * 1416000 / 3} = 708000 AU / \min/\sec dt$

Move Accel/Decel Constant Jerk = 3* Max Accel/3 = 708000 AU/min/sec/sec

Based on previous projects the following are givens:

Slow and Fast Velocity Filters = 0ms Slow/Fast Velocity Threshold = 0 AU/minute Rollover Position = 0 AU Software Upper Limit = +100000 Software Lower Limit = -100000 Ignore Limits = Yes Resume able Estop Allowed? = No

Position Data:

Input Polarity = Negative Output Polarity = Negative Analog Output Offset = 0mv Feed Forward % = 0% Proportional Gain (Kp) = 2000 (AU/min)/(AUFE) Integral Gain (Ki) = 0 (AU/min)/(AUFE*min) Derivative Gain (Kd) = 0 (AU/min)/(AUFE/min) + Integral Error Limit = +100 - Integral Error Limit = -100 Following Error Limit = $(Counts / Motor \operatorname{Re} v)/8*(AU / LU)*(LU / FU))$ 4000*8*.250 = 125AUThis will be fine tuned on start up

Update rate for the axis = 1.0 ms

In Position Band = 10LU*(AU/LU) = 10 AU This will be fine tuned on start up

Note:

The servo file setup data is used to determine the movement of the proportional valve during operation. We do not enter values for voltage for moving the valve during different modes of operation. The motion controller uses the values entered above plus for certain moves we provide a position and a rate to the motion controller and it adjust the valve accordingly through its analog output to the valve.