To: P. Lin, P. Broberg and Mr. Joe Fortney

From: Gary Atchison
Date: 2/22/10
Re: Forming Die Test Press
Design Project Report

## Report Outline

- Report Summary
- Problems and Corrections
- Status of the Machine
- Timeline for Completion
- Supporting Information
- System Block Diagram
- Project Gantt Chart
- Hydraulic Power Unit Calculations
- Motion Controller Information Calculations


## Report Summary

Gentlemen, what you will find in the following report are updated screen shots of my project Gantt chart, the system calculations for the hydraulic power unit required for the machine and the MMC Standalone control setup file calculations. Also is a brief description of any issues that have come up along the way and their corrections, what is the status of the machine and what is left to be done. I would like to note that this machine has had an Ethernet module installed on the MMC Standalone control that will allow us to connect remotely from Marion with the machine in Germany. This will allow us to be able to modify and download control programs if needed without making a trip to Germany.

## Problems and Corrections

The original electrical design of the machine was done a year ago before the hydraulic system was designed so the intention was to use the hydraulic system design of the first test press machine. It did not have a cooling fan motor on the hydraulic unit. Instead it used 2 electrical enclosure cooling fans mounted around the hydraulic unit to help cool it. Because we wanted to improve the design of the hydraulic power unit a cooling fan was included so we had to update the electrical design to include the hydraulic power unit cooling fan.

Another problem that has arose because of the changing the hydraulic power unit design from that of the original test press design is with the new design we changed from a hydraulic servo valve which uses a current input to a proportional valve which uses a voltage input. Because of this, the electrical system has been updated which requires another 24 V power supply for the proportional valve and the removal of the VC2124 which was going to be used to convert the analog $+/-10 \mathrm{~V}$ signal to a current which the servo valve used. We are currently awaiting the
arrival of the power supply so it can be installed. At that time we will remove the VC2124 converter and complete the wiring as necessary.

There was some confusion when parts were ordered for the hydraulic system and the wrong length cylinder and linear transducer were ordered. Parts were ordered for a 10 inch cylinder instead of a 15 inch cylinder. A 15 inch cylinder and a 15 inch MTS linear transducer have been ordered and are expected to arrive any time.

## Status of the Machine

Presently the machine has been built allowing the installation of the hydraulic power unit and the electrical enclosure. Hoses are being routed to length so that they can be crimped. The safety pin cylinder has been installed and guards are in the process of being installed. Most of the electrical installation has been done but does not include the installation of the outputs solenoids for air control. The MS Project Gantt chart has been updated to reflect the recent progress on the machine and a document containing the calculations for the hydraulic power unit and the motion control system has been created.

What is left to be done is to complete the hydraulic hose installation and the machine wiring at which time we can begin installing the programs for the operation of the machine. Once these are complete we can begin testing and debug of the various systems. Once testing and debug are complete we can fully run the machine to make sure that all requirements have been met.

## Time Line for Completion

Present: 2/19/10
Finish electrical and hydraulic installation: 3/1/10
Finish the installation of interlocks and guards: 3/1/10
Testing and Debug complete by: 3/15/10
Ship the Machine: 3/15/10 to 4/15/10 depending on machine schedule

## Supporting Information

What you will find in the following information is the information for the system design, including hydraulic and motion control calculations. These will be included in the final report at the end of the semester. You will also find a block diagram that shows the basic system components and how they are connected to create a complete system. The only updated Gantt chart that will be shown are those with recent activity and those to yet be completed. I will begin on the next page with the System Block Diagram and I will provide subheadings for clarity.

## System Block Diagram:



Figure 1 System Block Diagram showing interconnectivity of all components

## Gantt Charts：

|  | 0 | Task Name | Duration | Start | Finish | Resource Names |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $\checkmark$ | $\square$ Analysis | 30 days | Mon 2／9／09 | Thu 3／19／09 |  |
| 2 | $\checkmark$ | $\square$ Analyze Existing Program | 1 day | Mon 2／9／09 | Mon 2／9／09 | Gary Atchison，Roger Beck |
| 3 | $\checkmark$ | Review Controls and VO Opertion in Existing Sequential Code | 1 day | Mon 2／9／09 | Mon 2／9／09 | Gary Atchison |
| 4 | $\checkmark$ | $\square$ Analyze Existing Controls | 1 day | Mon 2／9／09 | Mon 2／9／09 | Gary Atchison［18\％］，Roger Beck |
| 5 | $\checkmark$ | Review Existing Controls Usage and Wiring Schematics to determine what is needed | 1 day | Mon 2／9／09 | Mon 2／9／09 | Roger Beck，Gary Atchison |
| 6 | $\checkmark$ | Compare Delta Computer System with G\＆L Controls MMC to determine brand of Controls | 1 day | Mon 2／9／09 | Mon 2／9／09 | Roger Beck，Gary Atchison |
| 7 | $\checkmark$ | $\square$ Order New Control System | 30 days | Mon 2／9／09 | Thu 3／19／09 | Gary Atchison［17\％］，Roger Beck |
| 8 | $\checkmark$ | Place order for control system components and electrical parts | 30 days | Mon 2／9／09 | Thu 3／19／09 | Gary Atchison，Roger Beck |
| 9 | $\checkmark$ | $\square$ Developing the New Control System | 38 days | Wed 2／11／09 | Wed 4／1／09 | Roger Beck，Gary Atchison |
| 10 | $\checkmark$ | Create New Electrical Drawings | 5 days | Tue 2／24／09 | Mon 3／2／09 | Roger Beck |
| 11 | $\checkmark$ | Create New Ladder Program | 21 days | Wed 2／11／09 | Tue 3／10／09 | Gary Atchison |
| 12 | $\checkmark$ | Mock Up Control System to test Communication | 1 day | Wed 4／1／09 | Wed 4／1／09 | Gary Atchison |
| 13 | $\checkmark$ | Progress Report 1 | 1 day | Thu 9／10／09 | Thu 9／10／09 | Gary Atchison |
| 14 | $\checkmark$ | Progress Report 2 | 1 day | Thu 10／1／09 | Thu 10／1／09 | Gary Atchison |
| 15 | $\checkmark$ | Progress Report 3 | 1 day | Thu 10／22／09 | Thu 10／22／09 | Gary Atchison |
| 16 | $\checkmark$ | Progress Report 4 Initial Proposal and 10 minute presentation | 1 day | Thu 11／19／09 | Thu 11／19／09 | Gary Atchison |
| 17 | $\checkmark$ | Final ECET 490 Report and Presentation | 1 day | Thu 12／10／09 | Thu 12／10／09 | Gary Atchison |
| 18 | $\checkmark$ | $\square$ Develop and Order Hydraulic System | 62 days | Thu 10／22／09 | Tue 1／12／10 | Joe Fortney，AJ Lindvall |
| 19 | $\checkmark$ | Create New Hyd Sytem Design | 18 days | Thu 10／22／09 | Fri 11／13／09 | A．Lindvall，Joe Fortney |
| 20 | $\checkmark$ | Order Hyd System | 45 days | Fri 11／13／09 | Tue 1／12／10 | A．Lindvall |
| 21 |  | $\square$ Building the Press and Installing Components | 25.38 days | Mon 1／11／10 | Thu 2／11／10 | Assembly Department，Electrical Department |
| 22 | $\checkmark$ | Paint the machine structure | 1 day | Mon 1／25／10 | Mon 1／25／10 | Assembly Department |
| 23 |  | $\square$ Build the Press | 14.75 days | Mon 1／25／10 | Thu 2／11／10 | Assembly Department |
| 24 | $\checkmark$ | Assemble the Forming Head | 1 day | Mon 1／25／10 | Mon 1／25／10 | Assembly Department |
| 25 | $\checkmark$ | Install Brass Forming Head to Guide Pin Bushings | 1 day | Fri 2／5／10 | Fri 2／5／10 | Assembly Department |
| 26 | 国 | Install Guards and Interlocking Mechanisms | 2 days | Mon 2／8／10 | Tue 2／9／10 | Assembly Department |
| 27 | 國 | Install air solenoids and Safety Axis Lock Cylinders | 2 days | Tue 2／9／10 | Wed $2 / 10 / 10$ | Assembly Department |
| 28 | 國 | Install Hydraulic Cylinder and Linear Transducer | 1 day | Tue 2／9／10 | Tue 2／9／10 | Assembly Department |
| 29 | 國 | Install Hydraulic Hoses，Check Valves any remaining components | 2 days | Wed 2／10／10 | Thu 2／11／10 | Assembly Department |
| 30 |  | $\square$ Install Electrical Components | 10.56 days | Mon 1／11／10 | Fri 1／22／10 | Electrical Department |
| 31 | $\checkmark$ | Install Electrical Components such as Switches and Relays | 2 days | Mon 1／11／10 | Tue 1／12／10 | Electrical Department |
|  | 0 | Task Name | Duration | Start | Finish | Resource Names |
| 32 | $\checkmark$ | Added Cooling Fan Output to Ladder code and Drawings | 1 day | Fri 1／22／10 | Fri 1／22／10 | Gary Atchison，Roger Beck |
| 33 | $\checkmark$ | Install Controis Components such as MMC，Ethernet Module，SAB，VO Blocks | 1 day | Wed 1／13／10 | Wed 1／13／10 | Electrical Department |
| 34 | $\checkmark$ | Install Heat Controls | 1 day | Thu 1／14／10 | Thu 1／14／10 | Electrical Department |
| 35 | $\checkmark$ | Install Operator interface | 1 day | Thu 1／14／10 | Thu 1／14／10 | Electrical Department |
| 36 | 國 | Run and attach all wiring | 3 days | Thu 1／14／10 | Mon 1／18／10 | Electrical Department |
| 37 | $\checkmark$ | $\square$ Progress Report Due January 25， 2010 | 1 day | Mon 1／25／10 | Mon 1／25／10 | Gary Atchison |
| 38 | $\checkmark$ | Updated Progress Report Due by 5：00pm 1－25－10 | 1 day | Mon 1／25／10 | Mon 1／25／10 | Gary Atchison |
| 39 | $\checkmark$ | Updated Flow Diagrams for clarity，created paint documents and inserted into the proposal | 1 day | Mon 1／25／10 | Mon 1／25／10 | Gary Atchison |
| 40 | $\checkmark$ | Added Summary，updated Table of Contents，added departments to Resources | 1 day | Mon 1／25／10 | Mon 1／25／10 | Gary Atchison |
| 41 | $\checkmark$ | Updated the MS Project Gantt Chart | 1 day | Mon 1／25／10 | Mon 1／25／10 | Gary Atchison |
| 42 | $\checkmark$ | $\square$ Finalized Report Due February 1， 2010 | 1 day | Mon 21／1／10 | Mon 2／1／10 | Gary Atchison |
| 43 | $\checkmark$ | Progress Report \＃1 Phase｜｜Due by 5：00pm 2－1－10 | 1 day | Mon 211／10 | Mon 2／1／10 | Gary Atchison |
| 44 | $\checkmark$ | Update，Breakdown further the MS Project Gantt Chart Information | 1 day | Mon 2／1／10 | Mon 2／1／10 | Gary Atchison |
| 45 | $\checkmark$ | Add summary for any new changes and or modifications，review requirments | 1 day | Mon 211／10 | Mon 2／1／10 | Gary Atchison |
| 46 | $\checkmark$ | Design Report（2nd Report）Due by 5：00pm 2－22－10 | 1 day | Mon 2／9／09 | Mon 2／9／09 | Gary Atchison |
| 47 |  | $\square$ Installing Hydraulics and Starting Up the Machine | 308.06 days | Mon 2／9／09 | Fri 3／19／10 | Assembly Department |
| 48 | $\checkmark$ | Install Hydraulic System to the Machine | 3 days | Mon 2／15／10 | Wed 2／17／10 | Assembly Department |
| 49 |  | $\square$ Setup New Control System | 308.06 days | Mon 2／9／09 | Fri 3／19／10 | Gary Atchison |
| 50 | 國 | Download Operator Interface Program | 1 day | Mon 3／1／10 | Mon 3／1／10 | Gary Atchison |
| 51 | 国 | Download the machine program（Ladder） | 1 day | Mon 3／1／10 | Mon 3／1／10 | Gary Atchison |
| 52 | 断 | Establish Communication with MMC remotely using PicPro for Internet Downloading | 1 day | Mon 3／1／10 | Mon 3／1／10 | Gary Atchison |
| 53 | $\checkmark$ 全 | Figure out Axis Setup Data for Motion Control（Accel，Decel，Velocity and Head Open Positions） | 3 days | Mon 3／8／10 | Wed 3／10／10 | Consultant，Gary Atchison |
| 54 | 国 | Test Operator interface Communication（is it communicating with the ladder） | 1 day | Tue 3／2／10 | Tue 3／2／10 | Gary Atchison |
| 55 | 国 | Test heat Control and setup parameters for the heat | 1 day | Wed 3／3／10 | Wed 3／3／10 | Gary Atchison |
| 56 |  | $\square$ Test／／O Operation | 1 day | Mon 2／9／09 | Mon 2／9／09 |  |
| 57 |  | Solenoid Operation（Top Die Air，Bottom Die Air） | 1 day | Mon 2／9／09 | Mon 2／9／09 |  |
| 58 |  | Pilot Light Operation（Power On，Run Mode，Manual Mode，Lock Pins Retracted，Lock Pins Extended） | 1 day | Mon 2／9／09 | Mon 2／9／09 |  |
| 59 |  | $\square$ Test Safety Systems（Guards） | 2.06 days | Thu 3／11／10 | Fri 3／12／10 | Gary Atchison |
| 60 | 国 | Test Guard Operation | 1 day | Thu 3／11／10 | Thu 3／11／10 | Gary Atchison |
| 61 | 田 | Test Palm Button Operation | 1 day | Thu 3／11／10 | Thu 3／11／10 | Gary Atchison |
| 62 | 田 | Test Operation of the Auto／Manual Mode Switch | 1 day | Thu 3／11／10 | Thu 3／11／10｜ | Gary Atchison $V$ |


|  | 3 | Task Name | Duration | Start | Finish | Resource Names |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 63 | 戒 | Can we only start the hydraulics in Manual Mode using the Simultaneous Press of the Palm Buttons？ | 1 day | Thu 3／11／10 | Thu 3／11／10 | Gary Atchison |  |
| 64 | 國 | Can the accumulator only be charged when the guards are closed？ | 1 day | Fri 3／12／10 | Fri 3／12／10 | Gary Atchison |  |
| 65 | 國 | Does the accumulator only charge in Auto Mode？ | 1 day | Fri 3／12／10 | Fri 3／12／10 | Gary Atchison |  |
| 66 | 國 | Do the safety Pins engage when the sliding guard door is opened？ | 1 day | Fri 3／12／10 | Fri 3／12／10 | Gary Atchison |  |
| 67 |  | $\square$ Test the 8 Operations of the machine as described in the flow diagrams | 3.13 days | Mon 3／15／10 | Wed 3／17／10 | Gary Atchison |  |
| 68 | 田 | Locking Pins Operation | 1 day | Mon 3／15／10 | Mon 3／15／10 | Gary Atchison |  |
| 69 | 國 | Going to Start Position | 1 day | Mon 3／15／10 | Mon 3／15／10 | Gary Atchison |  |
| 70 | 國 | Hydraulic Startup | 1 day | Mon 3／15／10 | Mon 3／15／10 | Gary Atchison | Gantt Chart Sheet 2 1－22－ |
| 71 | 國 | Homing the Machine | 1 day | Tue 3／16／10 | Tue 3／16／10 | Gary Atchison |  |
| 72 | 國 | Going to Start Position based on the Program Selected（1－4）from the HMM | 1 day | Tue 3／16／10 | Tue 3／16／10 | Gary Atchison |  |
| 73 | 戒 | Cycle Start（Machine Start） | 1 day | Tue 3／16／10 | Tue 3／16／10 | Gary Atchison |  |
| 74 | 盏 | Manual movement of the head（Jogging） | 1 day | Wed 3／17／10 | Wed 3／17／10 | Gary Atchison |  |
| 75 | 國 | Heat Control | 1 day | Wed 3／17／10 | Wed 3／17／10 | Gary Atchison |  |
| 76 | 國 | Test Motion Control and perform debug of motion control until proper control is established | 2 days | Thu 3／18／10 | Fri 3／19／10 | Gary Atchison |  |
| 77 | 國 | Test functionality of the overall systems for proper operation（All systems working together） | 1 day | Fri 3／19／10 | Fri 3／19／10 | Gary Atchison |  |
| 78 | 國 | Do we meet the requirements for Safety，EC，Electrical and System | 1 day | Fri 3／19／10 | Fri 3／19／10 | Gary Atchison |  |
| 79 | 國 | System Construction and Unit Testing Report（3rd Report） | 1 day | Mon 3／22／10 | Mon 3／22／10 | Gary Atchison |  |
| 80 | 國 | First Testing Report Due 5：00pm 4－5－10（4th Report） | 1 day | Mon 4／5／10 | Mon 4／5／10 | Gary Atchison |  |
| 81 | 国 | Second Testing Report Due 5：00pm 4－12－10（5th Report） | 1 day | Mon 4／12／10 | Mon 4／12／10 | Gary Atchison |  |
| 82 |  | $\square$ Progress Report and Design Review | 14.63 days | Tue 4／13／10 | Fri 4／30／10 |  |  |
| 83 | 國 | Final Report Writing | 4 days | Tue 4／13／10 | Fri 4／16／10 | Gary Atchison |  |
| 84 | 國 | Final Project and Presentation | 5 days | Mon 4／26／10 | Fri 4／30／10 | Gary Atchison |  |

Figure 2 Gantt Chart updated to show recent and future activity

## Hydraulic Power Unit Calculations：

The following given parameters will be used to make hydraulic calculations to simulate a production speed of 40 SPM：

Time to Retract $=350 \mathrm{~ms}$
Time to Extend $=350 \mathrm{~ms}$
Closed Dwell $=500 \mathrm{~ms}$
Note：
Because this machine does not run in a continuous mode，open dwell is not considered in the calculation for head speed．Time to retract plus time to extend plus closed dwell as noted yield a 50 SPM machine rate．If we added an open dwell of 300 ms then it would be equal to a 40SPM machine．

Head Open Position 11.375 inches - Die Shut Height 7.25 inches $=4.125$ inch head stroke
Forming Pressure required $=20,000$ pounds forming force
Head weight with components $(H W)=1250$ pounds head +110 pounds components $=1360$ pounds

Friction Force $(\mathrm{FF})=.24^{*} \mathrm{HW}^{*} \cos \left(0^{\circ}\right)=.24^{*} 1360 * 1=326.4$ pounds

The pages following are the calculations to be used in the development of the Forming Die Test Press based on the above given conditions：

AverageVelocity $(V a)=4.125 i n c h e s / .350 \mathrm{~ms}=11.78$ inches $/ \mathrm{sec}$ ond
FinalVelocity $(V f)=2 * S \div t=(2 * 2.0625$ inches $) \div .175 \mathrm{sec}=23.6$ inches $/$ sec ond Using the distance and time under acceleration

Where S = Distance moved in inches $=2.0625$ inches
$\mathrm{t}=$ Time of acceleration $=.175$ seconds


## Maximum Oil Flows:

Cylinder Bore $=3.25$ inches
Cylinder Rod $=2$ inch diameter
CRA $=$ CylinderRodArea $=\pi * r^{2}=3.14 * 1.0^{2}=3.14$ inches $^{2}$
CPAE $=$ CylinderPistonAreaExtending $=\pi^{*} r^{2}=3.14 * 1.62$ inches $^{2}=8.3$ inches $^{2}$
$C P A R=$ CylinderPistonArea Retracting $=C P A E-C R A=8.3$ inches $^{2}-3.14$ inches $^{2}=5.16$ inches $^{2}$

## Oil Flow to Extend (OFE):

$O F E=C P A E * V f=\left(8.3 \mathrm{in}^{2} * 23.6 \mathrm{in} / \mathrm{sec}\right)=\left(195.9 \mathrm{in}^{3} / \mathrm{sec}\right) *(60 \mathrm{sec} / \mathrm{min})=$ $\left(11754 \mathrm{in}^{3} / \mathrm{min}\right) /\left(231 \mathrm{in}^{3} / \mathrm{gal}\right)=50.9 \mathrm{gal} / \mathrm{min}$

## Oil Flow to Retract (OFR):

$O F R=C P A R * V f=\left(5.16\right.$ inches $\left.^{2} * 23.6 \mathrm{in} / \mathrm{sec}\right)=\left(121.8\right.$ inches $\left.^{3} / \mathrm{sec}\right) *(60 \mathrm{sec} / \mathrm{min})=$ $\left(7308 i n c h e s^{3} / \mathrm{min}\right) /\left(231 i^{2} \mathrm{inch}^{3} / \mathrm{gal}\right)=31.6 \mathrm{gal} / \mathrm{min}$

Hydraulic Oil Pressure Required to generate 20,000 pounds of forming force (HOPR):
$H O P R=$ For min $g$ Force Required $/ C P A E=20000 / 8.3$ inches ${ }^{2}=2410$ pounds $/$ inches $^{2}$
Weight of the Head and Components (HW) + Friction Force (FF)
$\mathrm{HW}+\mathrm{FF}=1360$ pounds +326.4 pounds $=1686.4$ pounds
Find the amount of hydraulic pressure required to accelerate the head upward (PAHU):
To accelerate the 1686.4 pounds of the head at a production speed: "Use the formula"
a = acceleration rate
S = distance moved in inches
$t=$ time of acceleration in seconds
$a=(2 * S) / t^{2}$
$a=(2 * 2.0625$ inches $) / .175 \sec ^{2}=134.7$ inches $/ \mathrm{sec}^{2}$

## Convert acceleration to feet/sec:

$a / 12$ inches $=\left(134.7\right.$ inches $\left./ \mathrm{sec}^{2}\right) / 12=11.23$ feet $/ \mathrm{sec}^{2}$
As well as knowing acceleration we also need to know (R) which is the Resultant Force On the Body. To find (R) use the following formula:
$\mathrm{R}=$ Resultant Force on the Body
$\mathrm{w}=\mathrm{HW}+\mathrm{FF}$
$\mathrm{g}=$ Gravitational Force ( 32.16 feet $/ \mathrm{sec}^{2}$ ) or ( 9.81 meters $/ \mathrm{sec}^{2}$ )
$\mathrm{a}=$ acceleration rate in feet $/ \mathrm{sec}^{2}$
$R=(w / g) * a=1686.4$ pounds $/\left(32.16 \mathrm{ft} / \mathrm{sec}^{2}\right)=52.4$ footpound $/ \mathrm{sec}^{2}$
( 52.4 footpound $\left./ \mathrm{sec}^{2}\right) *\left(11.23 \mathrm{ft} / \mathrm{sec}^{2}\right)=587.9$ pounds
$W=R+w=587.9$ pounds $+w=587.9+1686.4$ pounds $=2274.3$ pounds
To finish finding hydraulic pressure need to accelerate the head upward: Use the flowing formula for Pressure to Accelerate Head Upward (PAHU):
$P A H U=W / C P A R=(2274.3$ pounds $) /\left(5.16\right.$ inches $\left.^{2}\right)=441$ pounds $/$ in $^{2}$

Note:
Accumulator Pressure must be greater than or equal to the Forming Pressure (HOPR), which is 2410 pounds/inch ${ }^{2}$ because pressure is required from the accumulator for movement of the forming head.

To find the amount of pressure required for the accumulator pre-charge we must know and do the following:

1) The largest volume of oil taken from the accumulator will be at the maximum amount of head stroke (HS) which is:

Four head open positions will be needed:
20.375 inches
17.375 inches
14.375 inches
11.375 inches

Two different shut heights (closed die height) will be used for the dies:
12 inch
7.25 inch

12 inch shut height will be used with the 20.375 inch and 17.375 inch Machine Head Open Position
7.25 inch shut height will be used with the 14.375 inch and 11.375 inch Machine Head Open Position

The greatest head travel is realized when using the 20.375 inch Head Open Position with the 12 inch shut height die, so;

HS $($ HeadStroke $)=$ 20.375inch -12 inch $=8.375$ inches
2) The oil volume required from the accumulator to move the head 8.375 inches is found by the following:

## Extending:

HS ${ }^{*} C P A E=8.375$ inch $^{*} 8.3$ in $^{2}=69.5$ in $^{3}$
This 69.5 inches $^{3}$ is compressed to 2410 pounds/inch ${ }^{2}$
We need to know that $.5 \%$ oil volume compression/1000 psi is:
2410 psi $/ 1000$ psi $/ .005=2.41 * .005=1.205 \%$ or .01205
Now we can finish finding oil volume from the accumulator (OFA) to move the head 8.375 inches
$O F A=(H S * C P A E) * .01205=.84 i n^{3}+(H S * C P A E)=70.34 i n^{3}$
$O F A=69.5 * .0125=.84+69.5=70.34 \mathrm{in}^{3}$

Now we can find the amount of pressure required for the accumulator pre-charge
Use the equation:
$P_{1} * V_{1}=P_{2} * V_{2}$
Where:
$\mathrm{P}_{1}=H O P R=2410$ pounds $/$ inches $^{2}$
$\mathrm{P}_{2}=$ Accumulator Pre-charge Pressure
$\mathrm{V}_{1}=$ Rated Gas Volume $=1124$ in $^{3}$
$\mathrm{V}_{2}=V_{1}-O F A=1124 \mathrm{in}^{3}-70.34 \mathrm{in}^{3}=1053.7 \mathrm{in}^{3}$
$P_{2}=\left(P_{1} * V_{1}\right) / V_{2}=(2410 * 1124) / 1053.7=2708840 / 1053.7=2570.8 p s i$ Accumulator Pressure

PVR = Pump Volume Required at a 4.125" stroke
P = Pump = 4gallons $/$ minute
Stroke $=4.125$ inches
A = Cylinder Volume Extending
B = Cylinder Volume Retracting
$A=$ CPAE $*$ Stroke $=8.3$ inches $^{2} * 4.125$ inches $=34.24$ inches $^{3}$
$B=C P A R *$ Stroke $=5.16$ inches $^{2} * 4.125$ inches $=21.29$ inches $^{3}$
$P V R=A+B=34.24+21.29=55.53$ inches $^{3}$
$P V R$ Converted to gallons $=.24$ gallons
TTR = Time Required to Refill the Accumulator at a 4.125" stroke
$T T R=.24$ gallons required at .066 gallons/second (4gallonsl/minute) $=3.64 \mathrm{sec}$
M = Motor Size Required
$\mathrm{P}=$ Pump $=$ 4gallons $/$ minute
$\mathrm{P}_{2}=2571$ pounds/inches ${ }^{2}$
$\mathrm{K}_{1}=1714$
$\mathrm{K}_{2}=.85$
$\mathrm{M}=\frac{P_{2} * P}{K_{1} * K_{2}}=\frac{2571 * 4}{1714^{*} .85}=7.06$ HorsePower
We will use the common size 10 HorsePower motor

The volume of oil required to manually move the forming head at 1 inch/sec is as follows:
To manually extend the head:
1gallon $=231$ inches $^{3}$
CPAE * 1inch $=8.3$ inches ${ }^{3}$
8.3inches ${ }^{3} / 231$ inches $^{3}=.036$ gallons $/$ sec ond
(.036gallons / sec ond $) *(60 \mathrm{sec}$ onds $/ 1)=2.16$ gallons $/$ min ute

Using a 4-gallons/minute pump, the velocity that can be achieved manually extending the head 1inch/second:

4 gallons $/$ min ute $/ 2.16$ gallons $/$ minute $=1.85 i n c h e s /$ sec ond
To manually retract the head:
1gallon $=231$ inches $^{3}$
$C P A R *$ inch $=5.16$ inches $^{3}$
5.16inches ${ }^{3} /$ 231inches $^{3}=.023$ gallons $/$ sec ond
(.023gallons / sec ond $) *(60 \mathrm{sec}$ onds $/ 1)=1.34$ gallons $/$ min ute

Using a 4 gallons/minute pump, the velocity that can be achieved manually retracting the head 1inch/second:
$4 \mathrm{gpm} / 1.34 \mathrm{gpm}=2.98$ inches $/$ sec ond

## Motion Controller Information Calculations:

The setup information for the motion controller to make its calculations requires the following input data.

Resolution to be used for calculations $=.00025$ inch

## Axis Data:

Output Type = D/A
Input Type = Encoder
Output Slot Channel = 1.1
Input Slot Channel = 1.1
Encoder Driver = Differential
Encoder Type = Quadrature

## Scaling Data Requires:

Input Scaling:
Feedback Units $=4\left(4^{*}\right.$ resolution to $=.001 "$ of an inch $=4^{*} .00025=.001$ inch $)$
Ladder Units $=1(1 \mathrm{LU}=.001$ inch so values in the ladder to $=1$ inch are $* 1000)$

$$
\text { So } 4 \text { inches in the ladder }=4000
$$

Ladder Units/Axis Units = 1 (These are the units of measurement for the system and must be integers, at 1 no further scaling is needed)

## Output Scaling:

Commanded Voltage $=10000 \mathrm{mv}$ (This is equal to 10 V which is the analog signal the Controller outputs)
Motor RPM at Voltage = 23.6 inches/second or 1416 inches/minute (This is our calculated Vf)
Counts/Motor Rev = 4000 pulses/inch (Based on the resolution, 4000*. $00025=1$ inch)

## Iterator Data:

Velocity Limit $=\begin{aligned} & V f *(\text { Counts } / M t r \operatorname{Re} v) *(A U / L U) *(L U / F U) \\ & 1416 * 4000 * 1 *(1 / 4)=1,416,000 A U / \text { min ute }\end{aligned}$

Acceleration Ramp $=\begin{aligned} & \text { VelocityLimit } / t= \\ & 1416000 / .175=8,091,428 A U / \min \text { ute } / \text { sec } \text { ond }\end{aligned}$
Deceleration Ramp $=\begin{aligned} & \text { VelocityLimit } / t= \\ & 1416000 / .175=8,091,428 A U / \text { min } u t e ~\end{aligned}$ sec ond

Controlled Stop Ramp $=\begin{aligned} & \text { VelocityLimit } / t^{*} 10^{1}= \\ & 1416000 / .175=80,914,280 A U ~ / \text { min } u t e ~\end{aligned}$ sec ond

Move Accel/Decel Max Accel $=\begin{aligned} & (3 / 2) * \text { VelocityLimit } / 3 \text { sec } \text { onds }= \\ & (3 / 2) * 1416000 / 3=708000 A U / \mathrm{min} / \mathrm{sec}\end{aligned}$
Move Accel/Decel Constant Jerk = 3* Max Accel/3 = 708000 AU/min/sec/sec
Based on previous projects the following are givens:
Slow and Fast Velocity Filters $=0 \mathrm{~ms}$
Slow/Fast Velocity Threshold $=0$ AU/minute
Rollover Position $=0 \mathrm{AU}$
Software Upper Limit $=+100000$
Software Lower Limit $=-100000$
Ignore Limits = Yes
Resume able Estop Allowed? = No

## Position Data:

```
Input Polarity = Negative
Output Polarity = Negative
Analog Output Offset \(=0 \mathrm{mv}\)
Feed Forward \% = 0\%
Proportional Gain (Kp) = 2000 (AU/min)/(AUFE)
Integral Gain \((\mathrm{Ki})=0(\mathrm{AU} / \mathrm{min}) /(\mathrm{AUFE} * \mathrm{~min})\)
Derivative Gain \((\mathrm{Kd})=0(\mathrm{AU} / \mathrm{min}) /(\mathrm{AUFE} / \mathrm{min})\)
+ Integral Error Limit \(=+100\)
- Integral Error Limit = -100
\(\left.\begin{array}{rl}\text { Following Error Limit }= & (\text { Counts } / \text { Motor } \operatorname{Rev}) / 8 *(A U / L U) *(L U / F U) \\ & 4000 * 8 * .250=125 A U\end{array}\right)\)
```

Update rate for the axis $=1.0 \mathrm{~ms}$
In Position Band $=10 \mathrm{LU}(\mathrm{AU} / \mathrm{LU})=10 \mathrm{AU}$ This will be fine tuned on start up

Note:
The servo file setup data is used to determine the movement of the proportional valve during operation. We do not enter values for voltage for moving the valve during different modes of operation. The motion controller uses the values entered above plus for certain moves we provide a position and a rate to the motion controller and it adjust the valve accordingly through its analog output to the valve.

